

넥스트폼의 항공우주분야 개발 사례



2019. 09. 26



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열공력 솔버

1. 개발 사항



개발 사항

Pressure based

Incompressible

simpleN Foam
pimpleN Foam

Compressible

rhoSimpleFoam
rhoPimpleFoam
rhoCentralFoam

All speed range

Foundation
Extended

PCN Foam
pUCoupledCN Foam

Density based

Implicit LU-SGS
RoeFDS

Compressible

TSLAeroFoam

Combustion

Flamelet

pUCoupledFCN Foam

FlameMaster
Library Convert



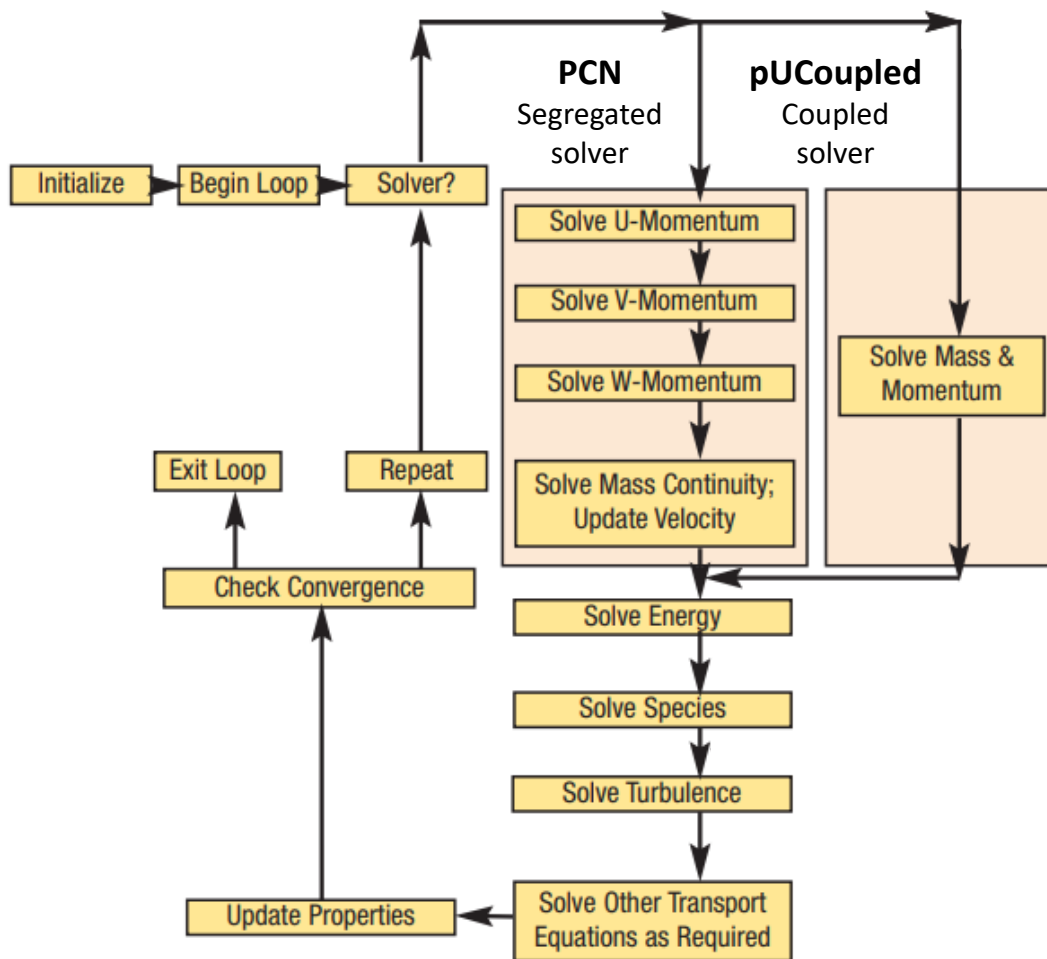


Pressure Based Compressible Solver

1. PCNFoam / pUCoupledCNFoam
2. Validation
3. Aerodynamic Performance
4. Practice Research



PCNFoam / pUCoupledCNFoam



- pressure based flux splitting central scheme
 - 격자 면에서의 flux 계산에 적용

$$\Psi_f \phi_f = \Psi_f^p (\alpha_f^p \phi_f^p + \alpha_f^p \phi_f^{min}) + \Psi_f^N (\alpha_f^N \phi_f^N - \alpha_f^p \phi_f^{min})$$

- Kurganov-Tadmor flux splitting scheme
 - Low Mach number correction
- Segregated 대비 압축성 영역 강건성
- 메모리 및 반복 시간 다소 손해



Validation

- 1D Lax problem



[초기]

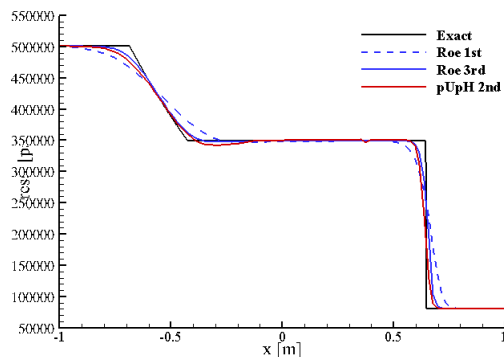


[종료]

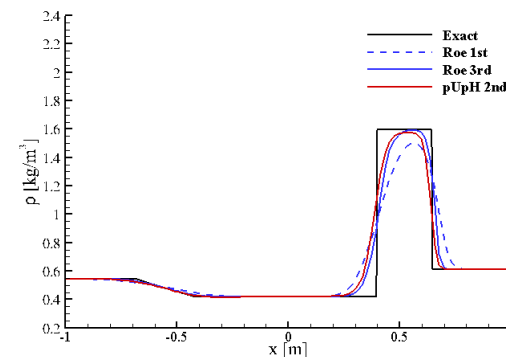
- Riemann Problem of Lax

- Shock tube problem with sever pressure
- Finial time: 0.13, Mesh points: 100
- Boundary condition: Extrapolation

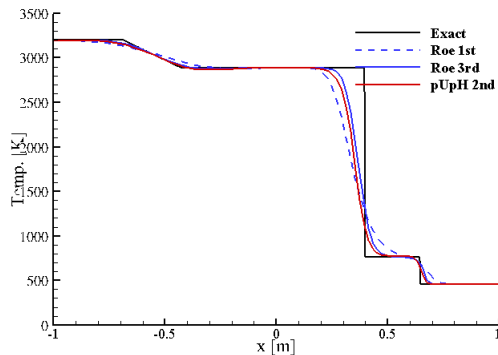
$$(\rho, u, p) = \begin{cases} (0.445, 0.698, 3.528) & \text{if } x \leq 0 \\ (0.5, 0, 0.571) & \text{if } x > 0 \end{cases}$$



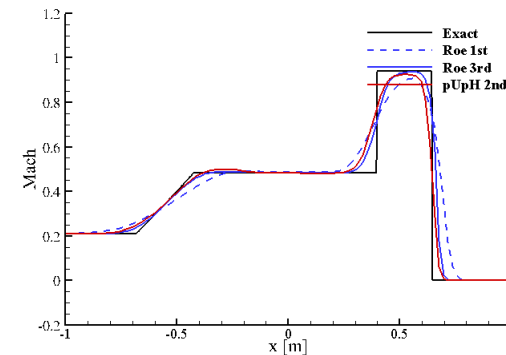
Pressure



Density



Temperature



Mach

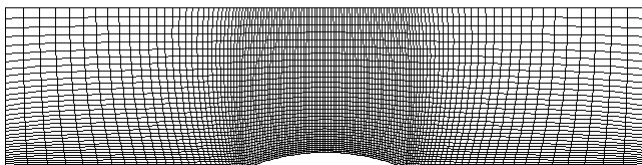


Validation

- 2D Euler 10% bump

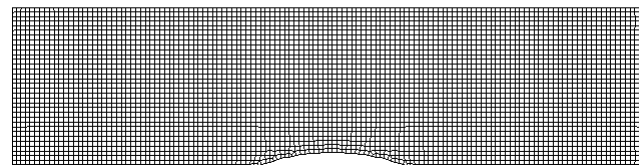
Precon./LM Roe FDS

Grid Size 121×35, Elliptic



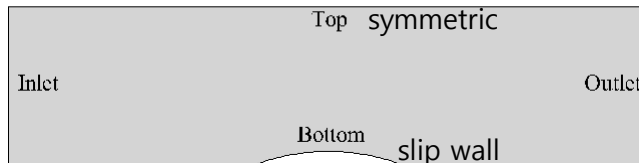
Present OpenFOAM

Grid Size 121×35, Salome, cfMesh



Boundary Name & Type

zerogradient



Subsonic: fixed value
Supersonic: zerogradient

Precon./LM Roe FDS

Solution Algorithm

Present OpenFOAM

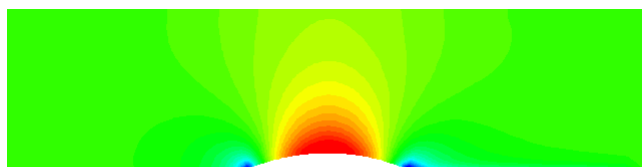
- Flux Scheme
 - Upwind type
 - Preconditioned Roe / LMRoe FDS
- Reconstruction Method
 - 2nd-order minmod limiter
- Integration Method
 - Fully Implicit LU-SGS

- Flux Scheme
 - 2nd-order Central difference type
 - Kurganov-Tadmor
- Reconstruction Method
 - minmod limiter
- Integration Method
 - Continuity: PCG
 - Moment. Energy: GMRES

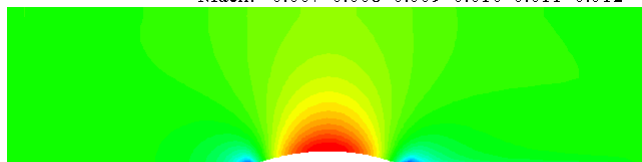
Validation

- 2D Euler 10% bump

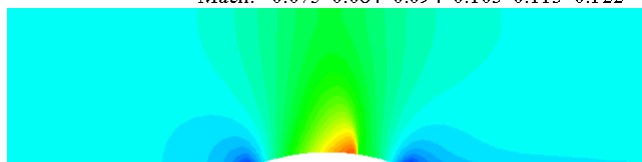
Preconditioned Roe FDS



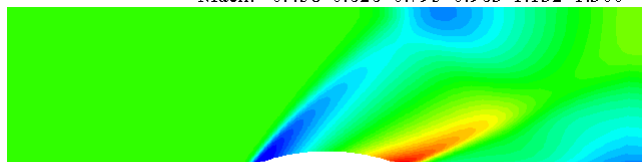
Mach: 0.007 0.008 0.009 0.010 0.011 0.012



Mach: 0.075 0.084 0.094 0.103 0.113 0.122

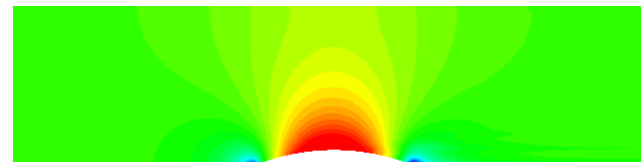


Mach: 0.458 0.626 0.795 0.963 1.132 1.300

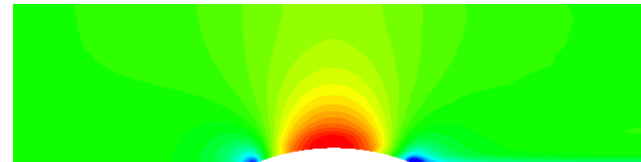


Mach: 1.400 1.620 1.840 2.060 2.280 2.500

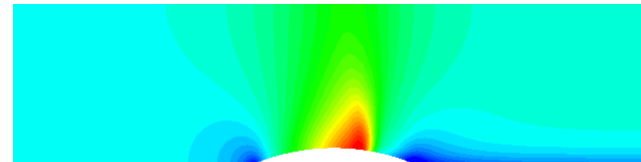
Present OpenFOAM



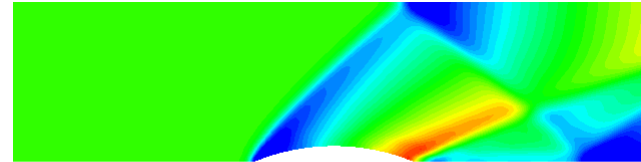
MaU: 0.007 0.008 0.009 0.010 0.011 0.012



MaU: 0.075 0.084 0.094 0.103 0.113 0.122



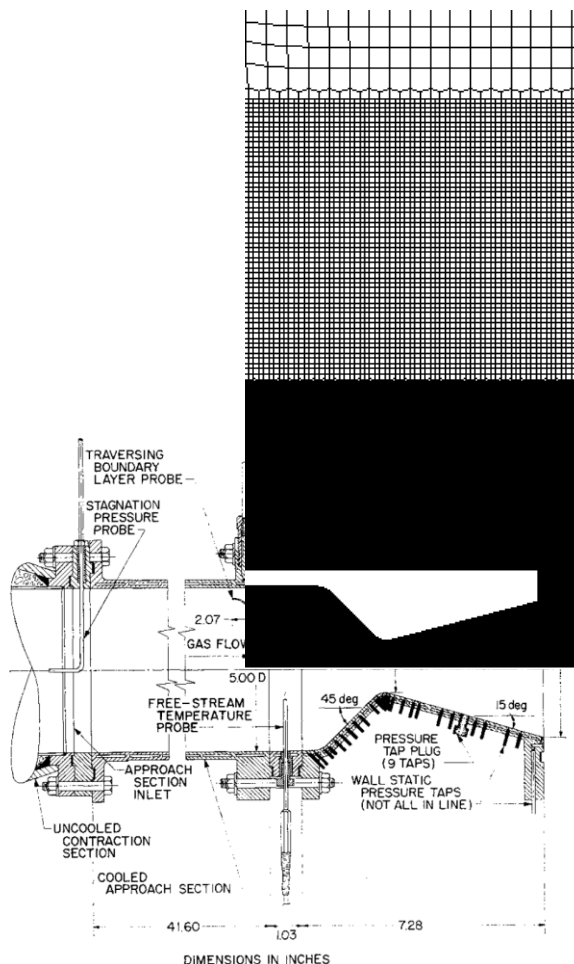
MaU: 0.458 0.626 0.795 0.963 1.132 1.300



MaU: 1.400 1.620 1.840 2.060 2.280 2.500

Validation

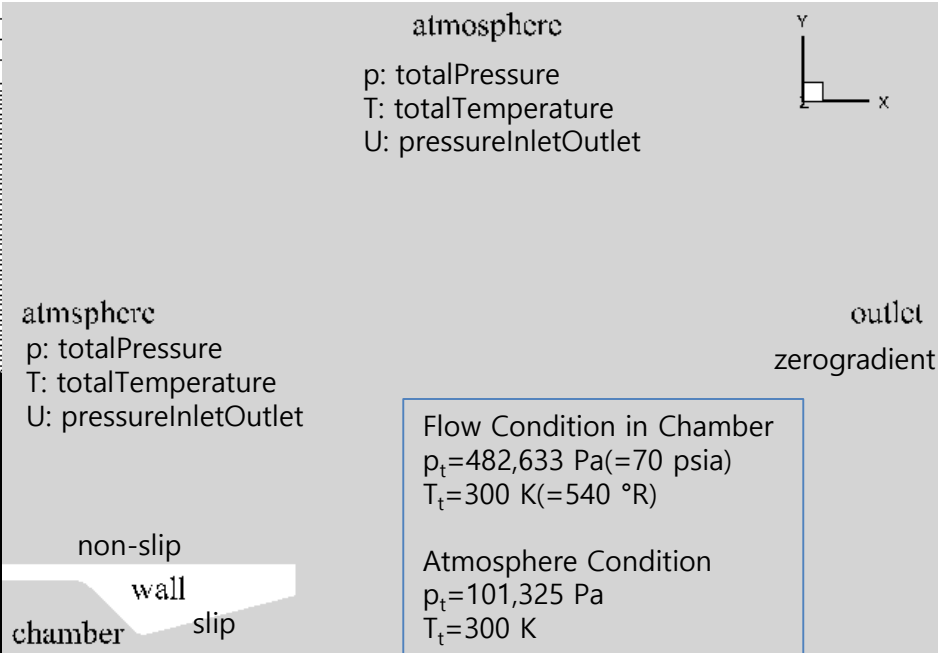
- JPL Nozzle Test



Experimental Configuration

Cuffel et al, AIAA Journal, Vol.7, No. 7, pp. 1364-1366, 1969

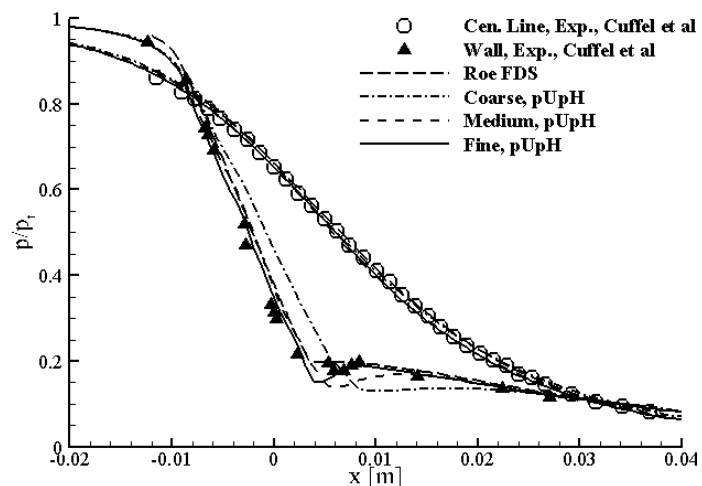
Boundary Name & Type





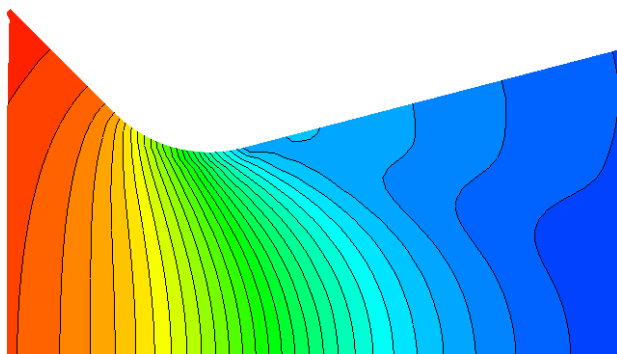
p: totalPressure
T: totalTemperature
U: pressureInletOutlet

- Flux Scheme
 - 2nd-order Central difference type
 - Kurganov-Tadmor
- Reconstruction Method
 - minmod limiter
- Integration Method
 - Continuity: PCG
 - Moment. Energy: GMRES

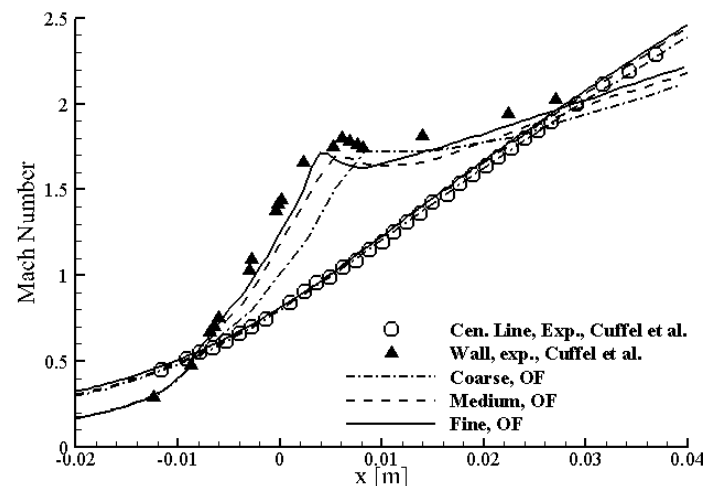
• JPL Nozzle Test





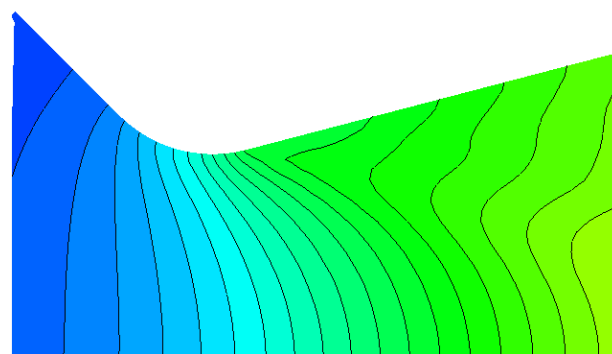
Pres. [MPa]: 0.01 0.10 0.20 0.29 0.39 0.48

Pressure Contour



Mach: 0.03 0.76 1.50 2.23 2.97 3.70

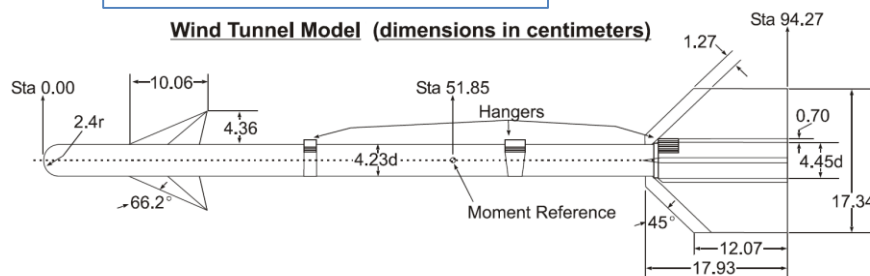
Mach Contour

Aerodynamic Performance

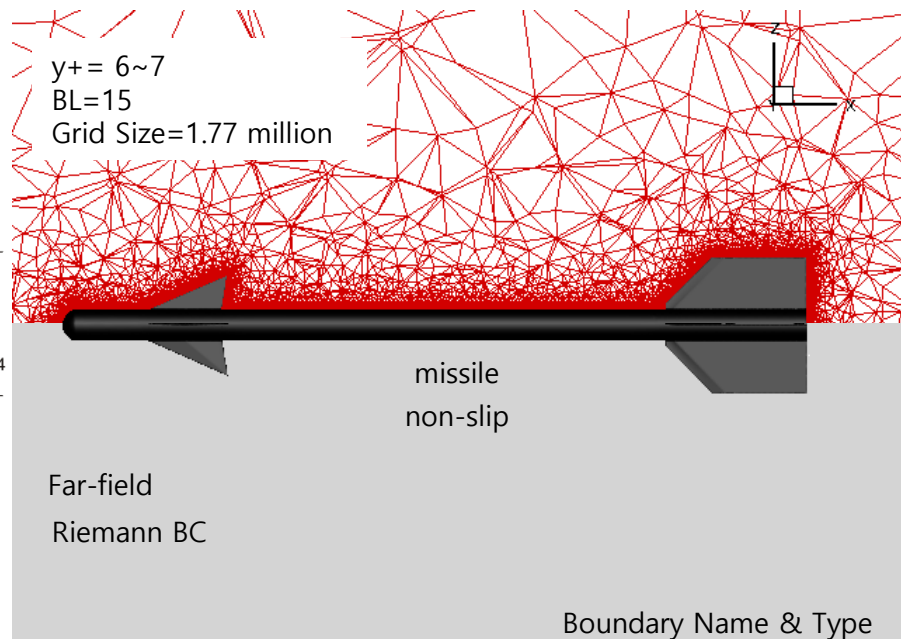
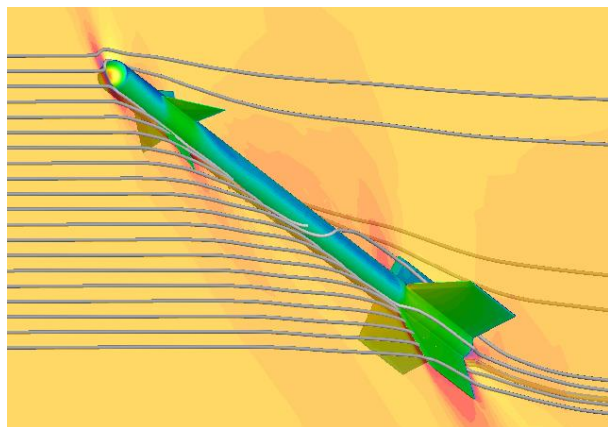
- Air-to-air Missile

Ref. Area= $1.408 \times 10^{-3} \text{ m}^2$
Max Body Dia.= $4.238 \times 10^{-2} \text{ m}$

Wind Tunnel Model (dimensions in centimeters)



Air-to-air missile dimension
Ernald et al, NASA TM X-3070, 1974



- Wind Tunnel Condition

- $Rex=6.56 \times 10^6$
- $T_t=332 \text{ K}$

- Far-field Condition

- AOA Sweep ($-5^\circ \sim 25^\circ$)

- M0.9

- $P=32.704 \text{ kPa}$
- $T=285.71 \text{ K}$
- $U=304.97 \text{ m/s}$

- M1.2

- $P=22.068 \text{ kPa}$
- $T=257.76 \text{ K}$
- $U=386.22 \text{ m/s}$

- Flux Scheme

- 2nd-order Central difference type
- Kurganov-Tadmor

- Reconstruction Method

- minmod limiter

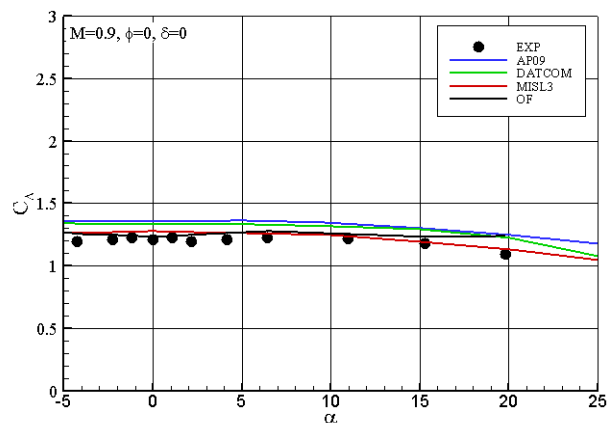
- Integration Method

- Continuity: PCG
- Moment. Energy: GMRES
- Turbulence: $k-\omega$ SST: BiCGStab

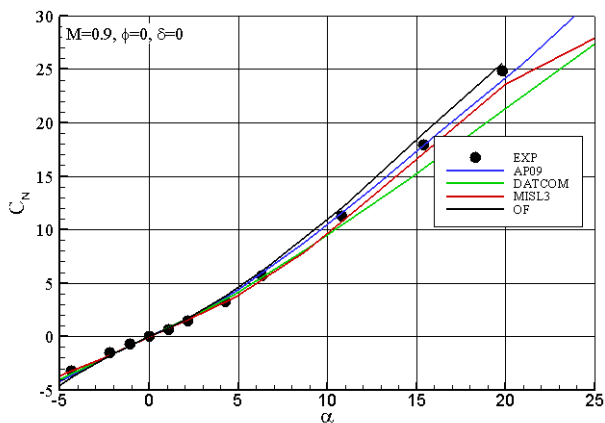


Aerodynamic Performance

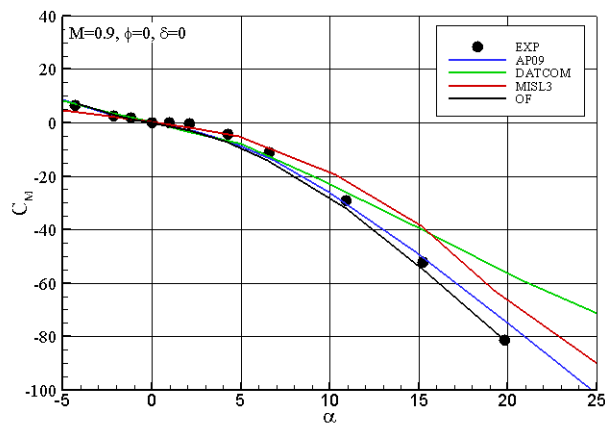
- Air-to-air Missile



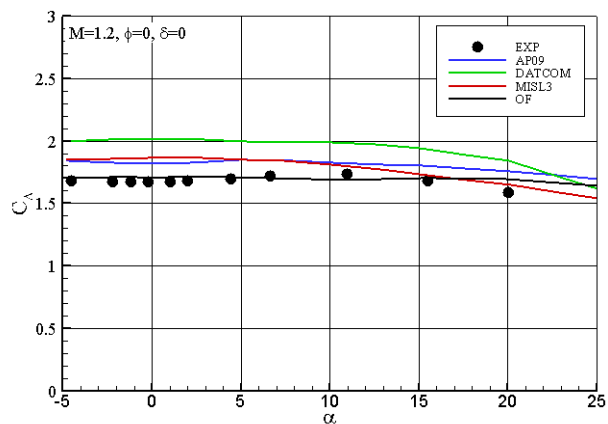
C_{L_r} M=0.9



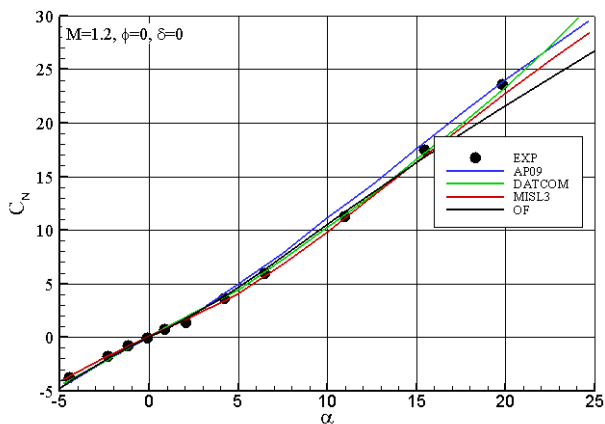
C_{N_r} M=0.9



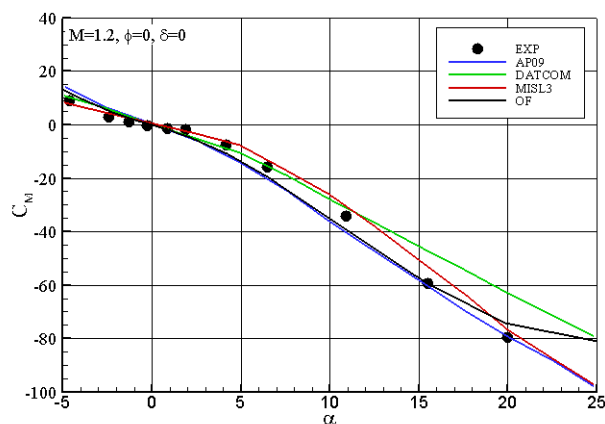
C_{M_r} M=0.9



C_{L_r} M=1.2



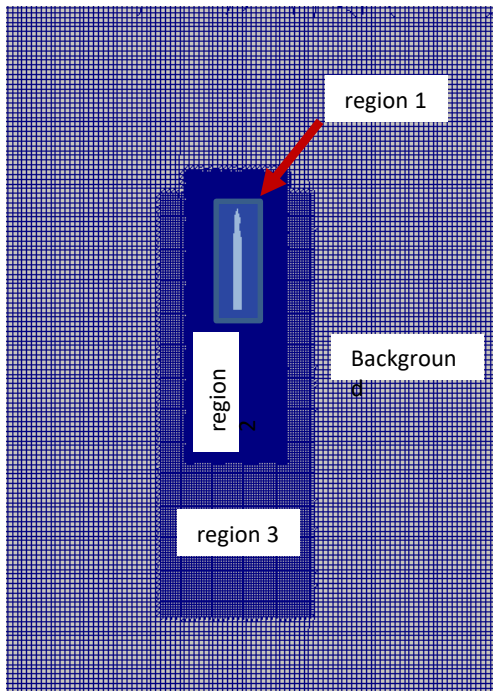
C_{N_r} M=1.2



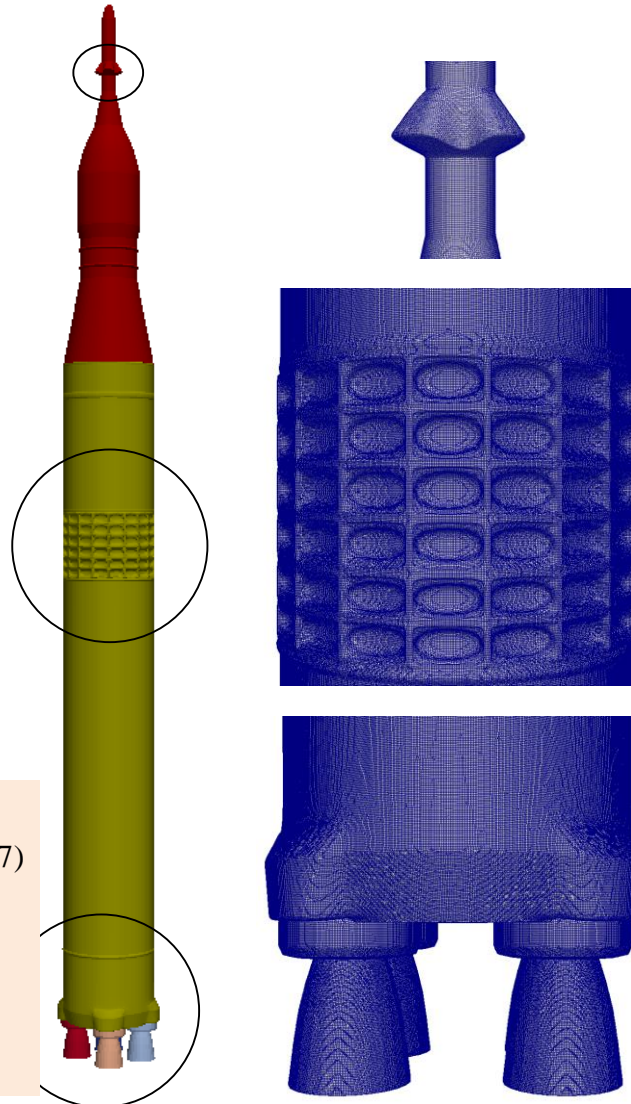
C_{M_r} M=1.2

Aerodynamic Performance

- SLS Launch Vehicle



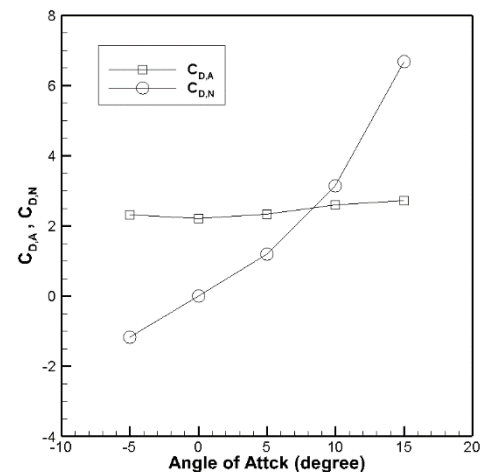
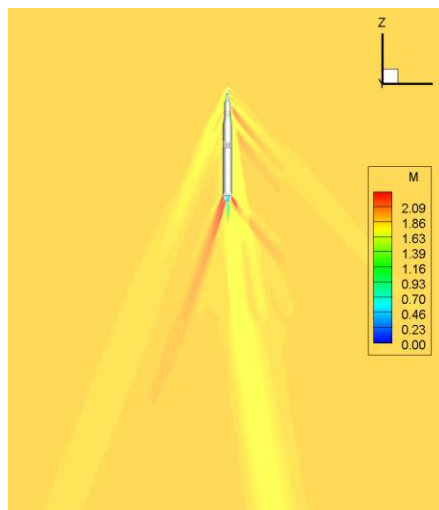
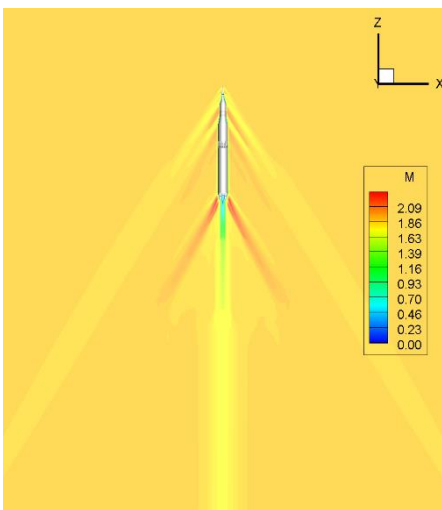
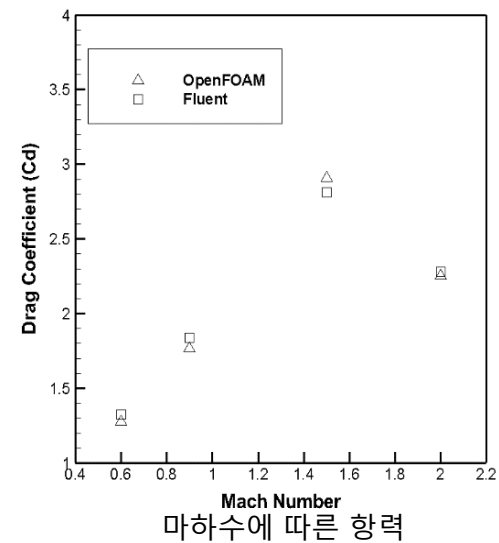
- Background: 8 m (level 0)
- Rocket Nozzle Surface: 0.0625m (level 7)
- 3 Refinement regions
 - Region 1 : 0.5m (level 4)
 - Region 2 : 2m (level 2)
 - Region 3 : 4m (level 1)
- 5 BL (first layer thickness = 0.003 m)



- Flux Scheme
 - 2nd-order Central difference type
 - Kurganov-Tadmor
- Reconstruction Method
 - minmod limiter
- Integration Method
 - Continuity: PCG
 - Moment. Energy: GMRES
 - Turbulence: $k-\omega$ SST: BiCGStab
- Far-field Condition
 - AOA Sweep ($-5^\circ \sim 15^\circ$)
 - Mach Sweep (0.6 ~ 2.0)

Aerodynamic Performance

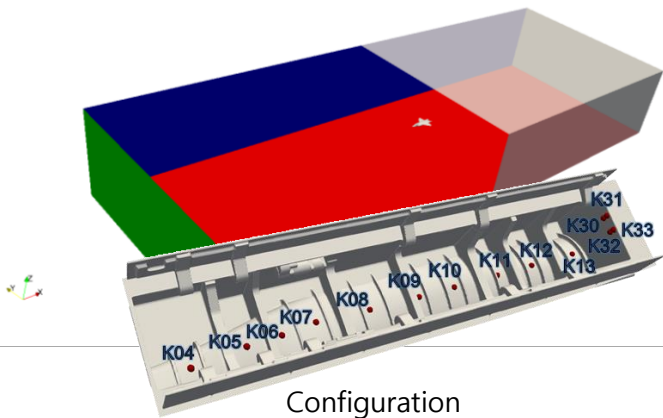
- SLS Launch Vel



AOA에 따른 공력계수

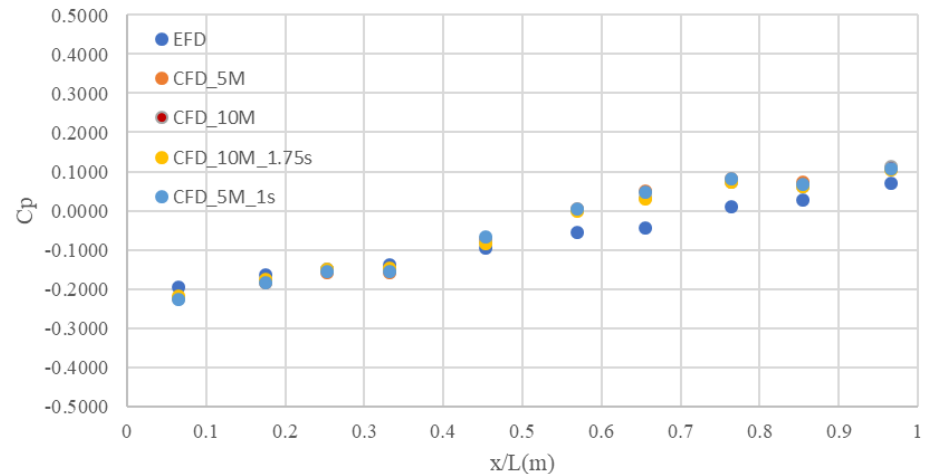
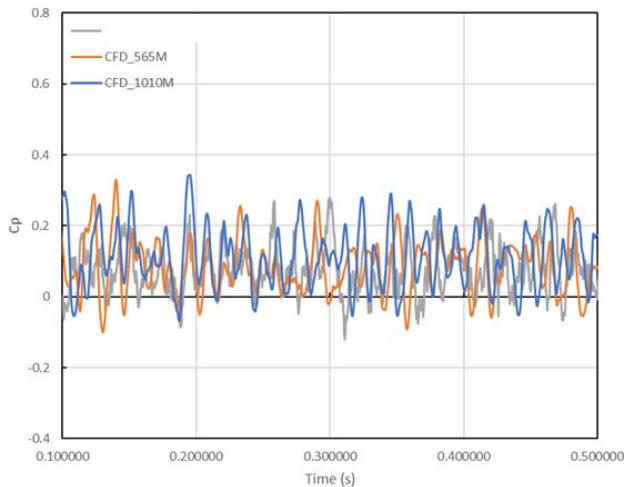
Practice Research

• 비행체 공동 유동



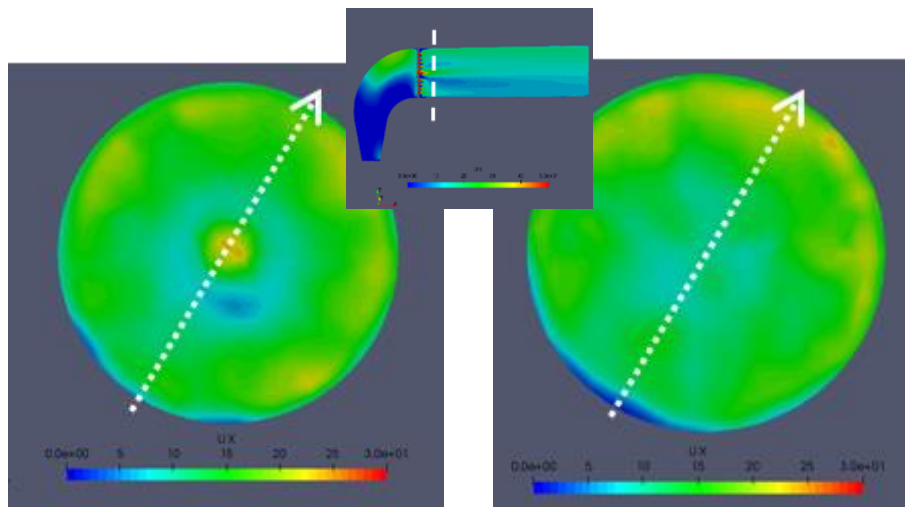
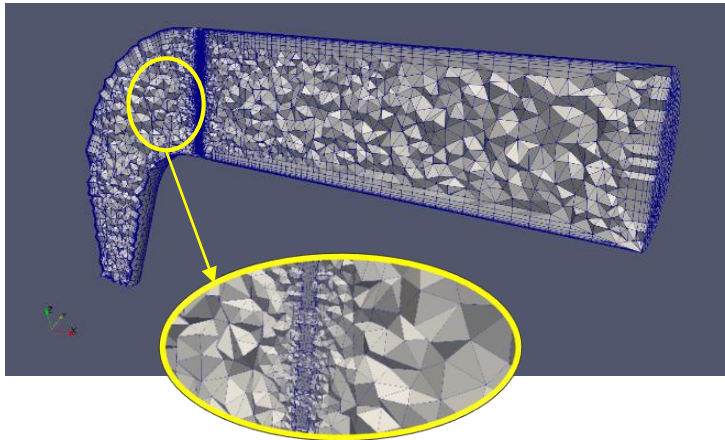
- 5.6 million polyhedral cells
 - $\Delta t=5e-5$
 - hexa: 5.4 M, poly: 0.21 M
- 10 million polyhedral cells
 - $\Delta t=4e-5$
 - hexa: 9.9 M, poly: 0.48 M

- Flux Scheme
 - 2nd-order Central difference type
 - Kurganov-Tadmor
- Reconstruction Method
 - minmod limiter
- Integration Method
 - Continuity: PCG
 - Moment. Energy: GMRES
 - Turbulence: k- ω SST: BiCGStab



Practice Research

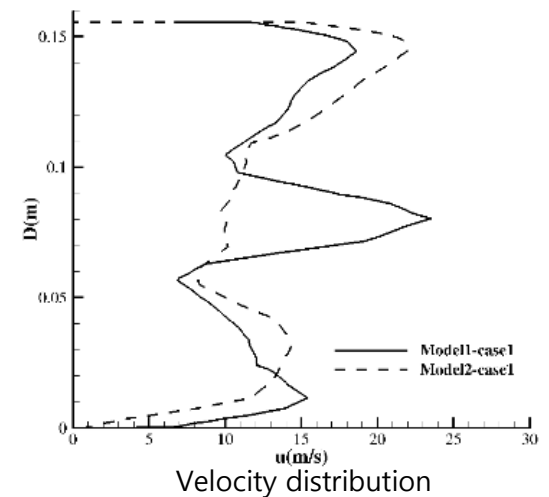
- KARI 산화제 유입부 유동



Model 1

Model 2

- Flux Scheme
 - 2nd-order Central difference type
 - Kurganov-Tadmor
- Reconstruction Method
 - minmod limiter
- Integration Method
 - Continuity: PCG
 - Moment, Energy: GMRES
 - Turbulence: realizable k- ϵ : BiCGStab
- Thermodynamics Properties
 - O₂



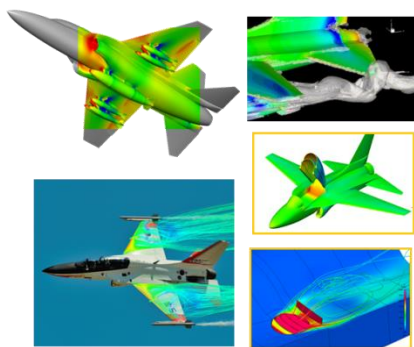


Density Based Compressible Solver

1. TSLAeroFoam

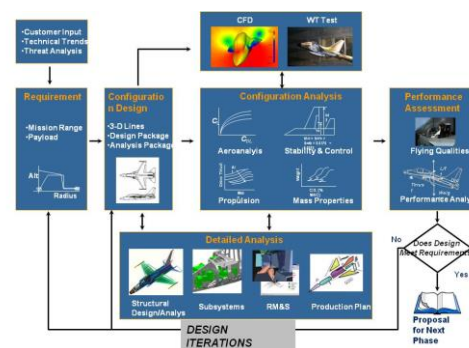
- Background

- Increasing CFD analysis to development phase
- Move problem resolution to massive computing in a design phase



Problem Resolution

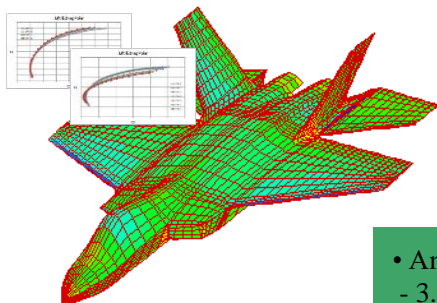
- Increasing CFD requirement



Design Phase Tool

- CFD Role

- Able to build up aerodynamic DB by using CFD



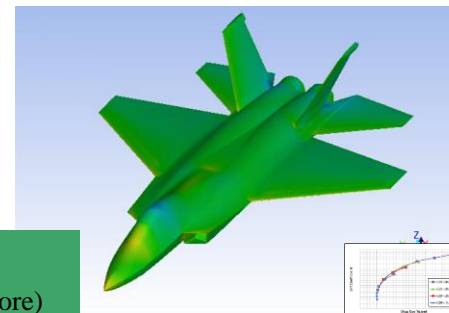
Panel Method

- Analysis condition: 2,185 cases
- AOA (13), SSA (5), M (11), δ (4)

- Analysis time
- 3.5 days



- Analysis time
- 121 days (32 core)
- 7.6 days (700 core)



CFD



TSLAeroFoam

- Governing Equations

- Favre-averaged Navier-Stokes Equation

$$\int_V \frac{\partial Q}{\partial t} dv + \int_{\partial V} (F_c - F_v) ds = 0 \quad W = \begin{bmatrix} \rho \\ \rho U \\ \rho E \end{bmatrix} \quad F_c = \begin{bmatrix} \rho U \\ \rho U_i U_j + PI \\ \rho H U \end{bmatrix} \quad F_v = \begin{bmatrix} 0 \\ \tau_{ij} \\ \nabla \cdot (\tau_{ij} U + \rho \alpha_{eff} \nabla h + (\mu + \frac{\mu_t}{\sigma_k}) \nabla k) \end{bmatrix}$$

- Turbulence Model

- Two equation k- ω Shear Stress Transport with wall function model

$$\frac{\partial(\rho k)}{\partial t} + \frac{\partial(\rho U_i k)}{\partial x_i} = \tilde{P}_k - \beta^* \rho k \omega + \frac{\partial}{\partial x_i} \left[(\mu + \sigma_k \mu_t) \frac{\partial k}{\partial x_i} \right]$$

$$\frac{\partial(\rho \omega)}{\partial t} + \frac{\partial(\rho U_i \omega)}{\partial x_i} = \alpha \rho S^2 - \beta \rho \omega^2 + \frac{\partial}{\partial x_i} \left[(\mu + \sigma_\omega \mu_t) \frac{\partial \omega}{\partial x_i} \right] + 2(1 - F_1) \rho \sigma_{\omega 2}$$

- Spatial Discretization

- Roe FDS
 - Reconstruction: Least square method

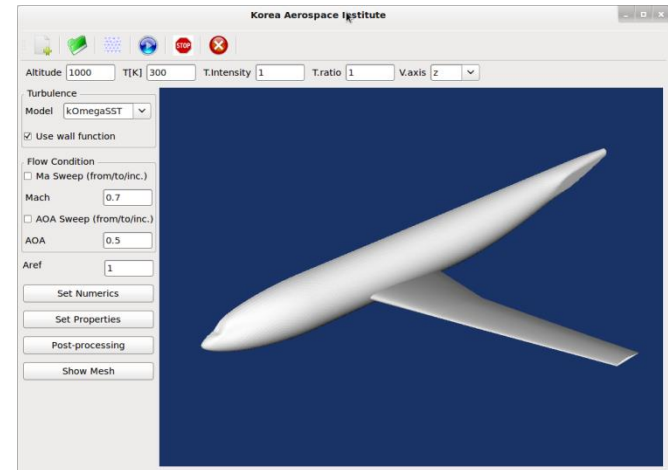
- Temporal Integration

- LU-SGS

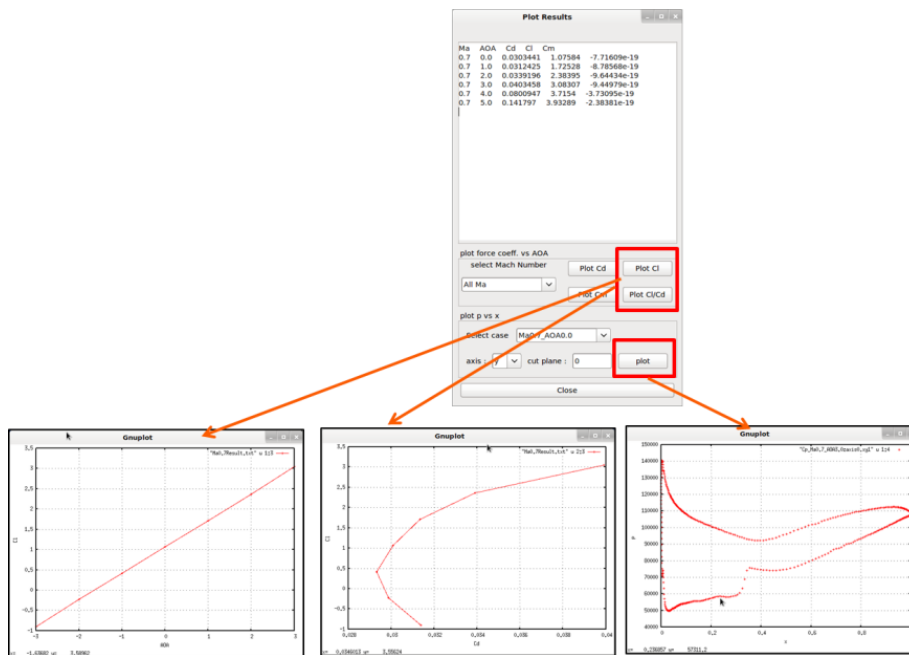


TSLAeroFoam

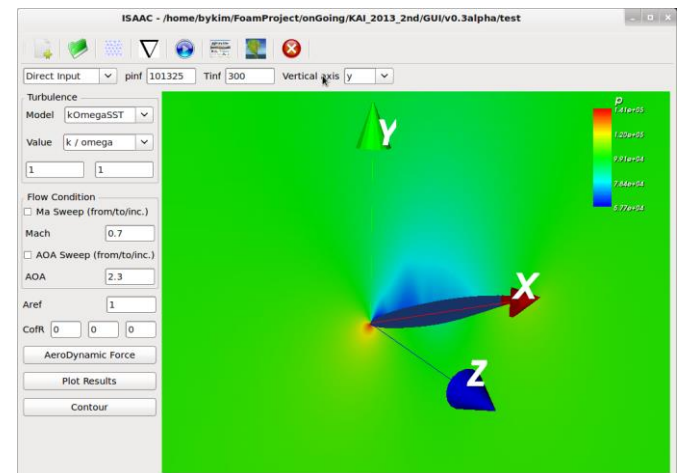
- Text User Interface
 - Batch job (e.g. Ma, AOA, SSA sweep)
- Graphic User Interface with 3D Graphic
 - Use VTK to generate mesh and contours



GUI graphic version



2D graphics post-processor



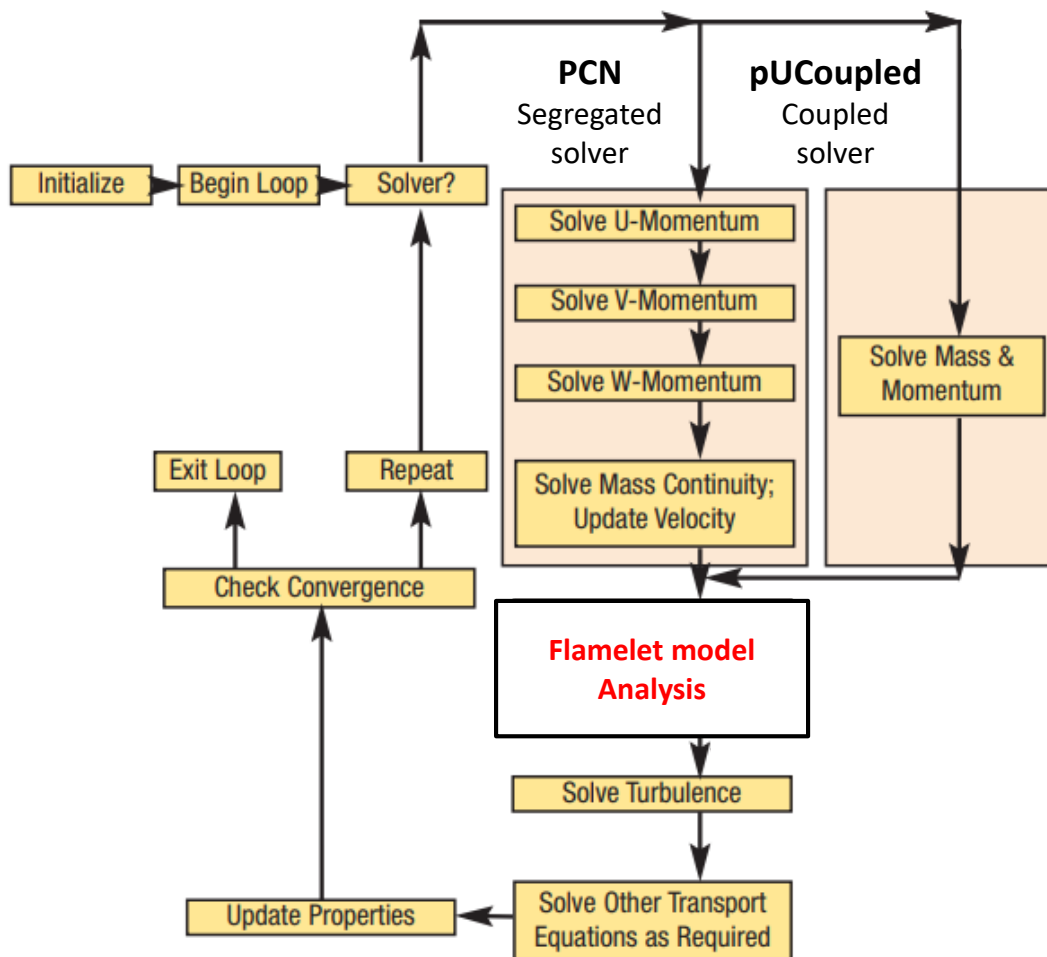
Embedded 3D graphic post-processor



Flamelet Solver

1. `pUCoupledFCNFoam`

pUCoupledFCN Foam



- pressure based flux splitting central scheme

– 격자 면에서의 flux 계산에 적용

$$\Psi_f \phi_f = \Psi_f^p (\alpha_f^p \phi_f^p + \alpha_f^p \phi_f^{min}) + \Psi_f^N (\alpha_f^N \phi_f^N - \alpha_f^p \phi_f^{min})$$

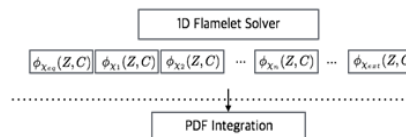
- Kurganov-Tadmor flux splitting scheme

– Low Mach number correction

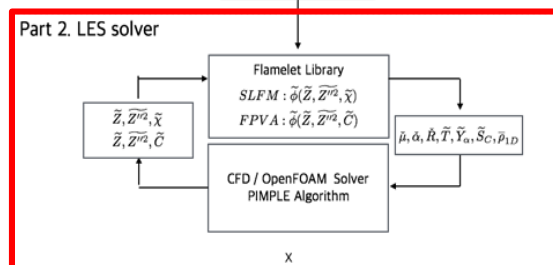
- Segregated 대비 압축성 영역 강건성

- 메모리 및 반복 시간 다소 손해

Part 1. flamelet library generation



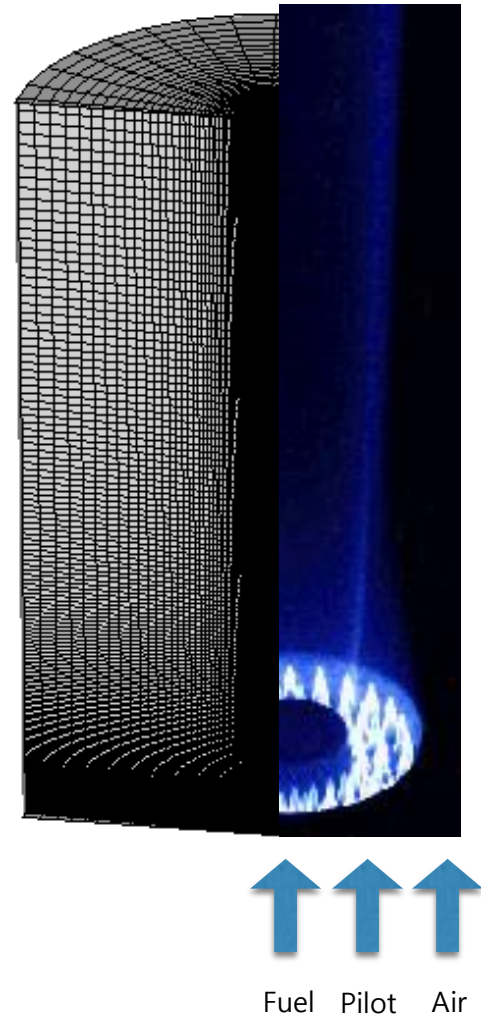
Part 2. LES solver



pUCoupledFCN Foam

- Flamelet Test [Piloted CH₄/air flame, SANDIA D]
 - Fuel : partially premixed CH₄(75%) and air(25%)
 - Oxidizer : air
 - Stoichiometric mixture fraction : 0.351
 - Reynolds number : 22400
- Dimension
 - Fuel nozzle diameter : 7.2 mm
 - Pilot nozzle diameter : 18.2 mm
- Pilot inlet condition
 - mixture fraction : 0.271
 - progress variable : 0.735
 - Temperature : 1880 K
- Turbulence model : Smagorinsky LES

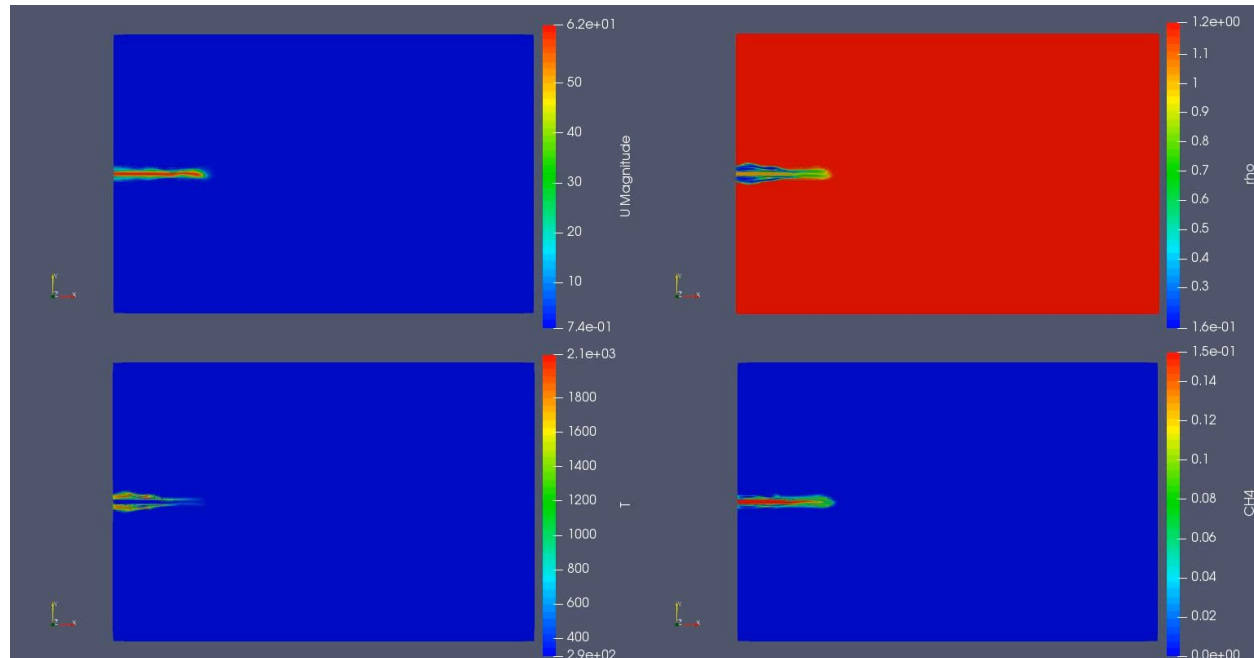
	Fuel	Pilot	Coflow
U [m/s]	49.6	11.4	0.9
T [K]	294	1880	291
Z	1	0.271	0





pUCoupledFCNFoam

- Flamelet Library
 - FLAMEMASTER
 - <https://www.itv.rwth-aachen.de/en/downloads/flamemaster/>
 - Methane global chemistry
 - $CH_4 + 2O_2 = CO_2 + 2H_2O$
 - GRI 3.0
 - Scalar dissipation rate
 - csv Table





Thank you for your attention